

FROM: $f_{B3B}(\alpha, \beta, v) = \frac{v - v_1}{v_2 - v_1} \left[c_0 + \frac{c_1 + c_2 \alpha + c_3 \alpha^2 + c_4 \alpha^3}{1 + c_5 \alpha} (1 + c_6 \beta) - c_7 + \frac{c_8 + c_9 \alpha + c_{10} \alpha^2 + c_{11} \alpha^3}{1 + c_{12} \alpha} (1 + c_{13} \beta) \right]$ [1]

THE B3B STRENGTH TEST

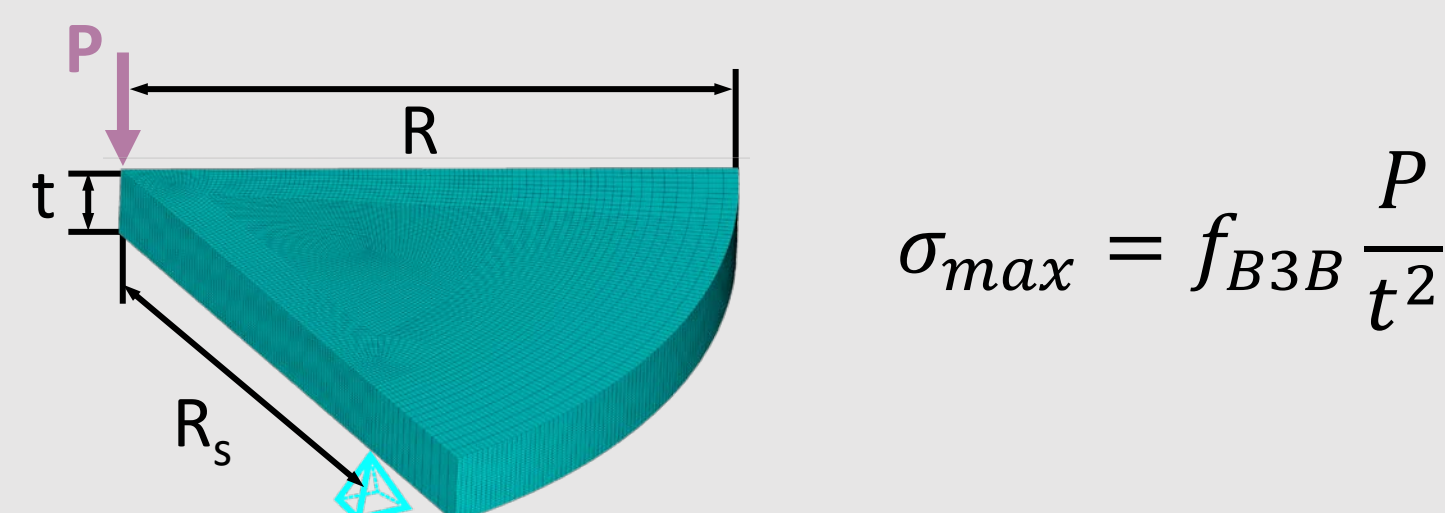
Extending and simplifying stress evaluation

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INTRODUCTION

The Ball-on-Three-Balls-Test (B3B) is a biaxial mechanical strength test with [2]:

- Flexible specimen size
- Easy handling and execution
- Low systematic error

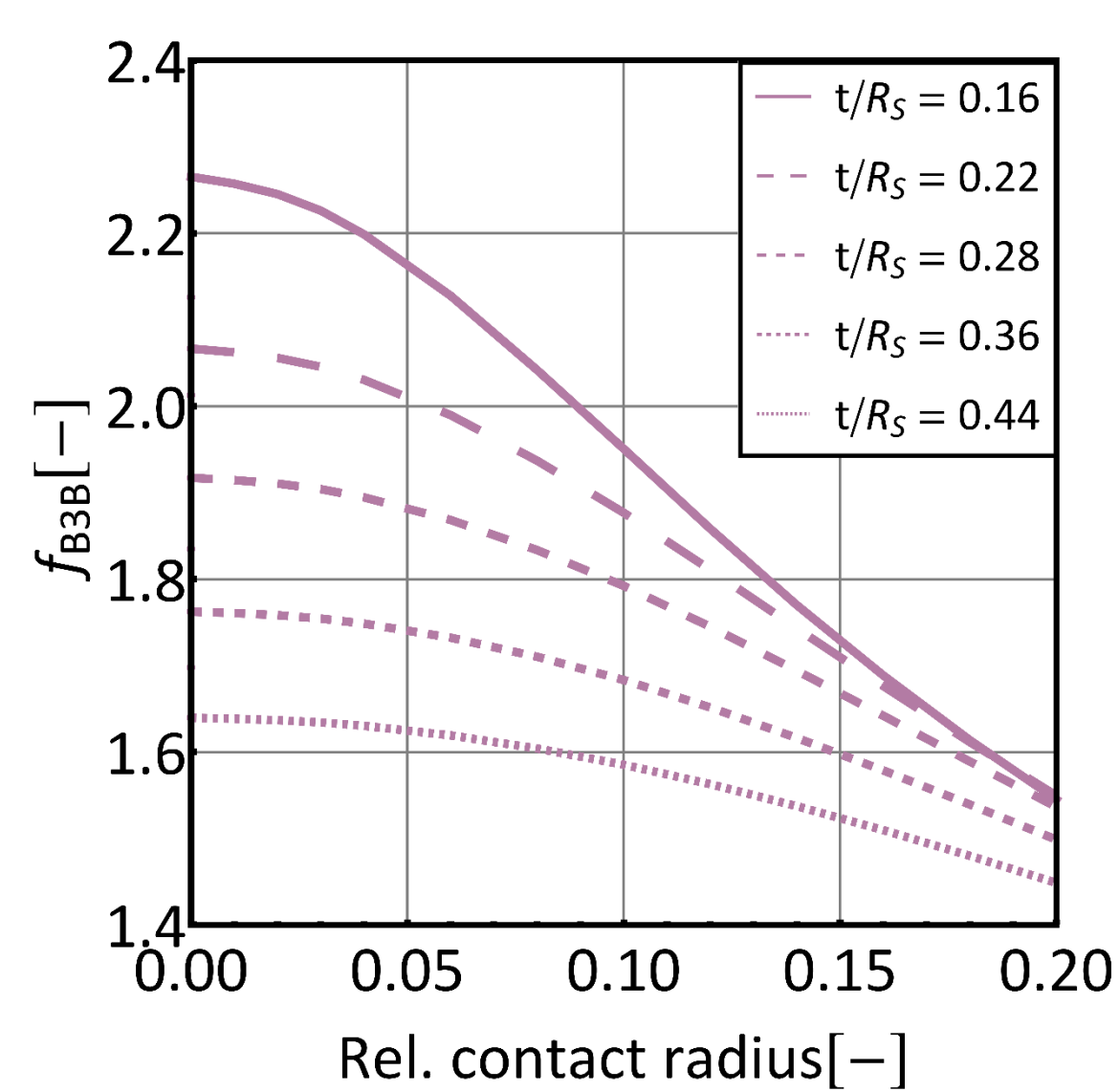


- No analytical solution
- Existing fit for f_{B3B} (top line) is unwieldy
- f_{B3B} is load-dependent at high loads

Aim

- Simplify fit for f_{B3B}
- Extend f_{B3B} to consider high loads

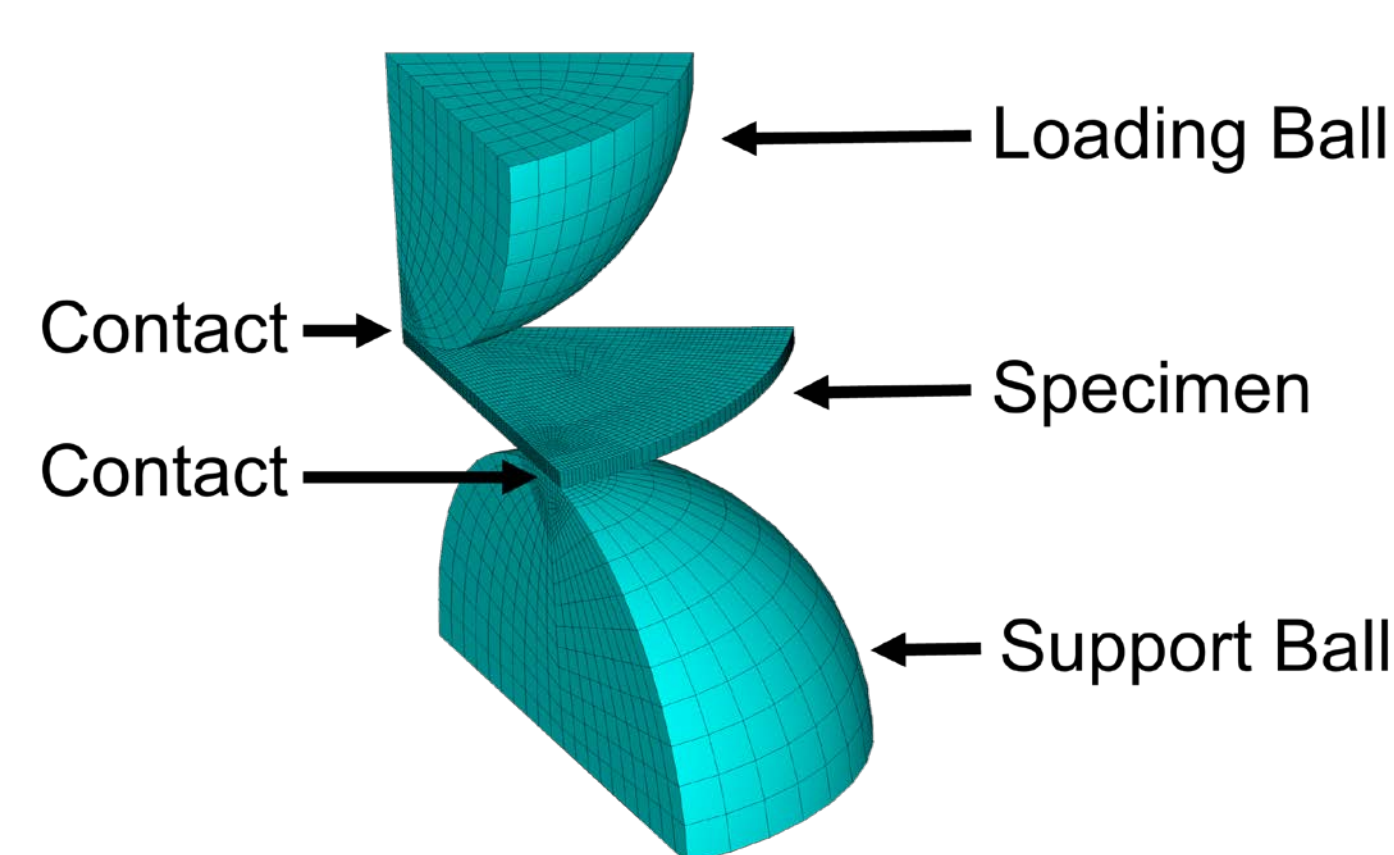
EXTENSION



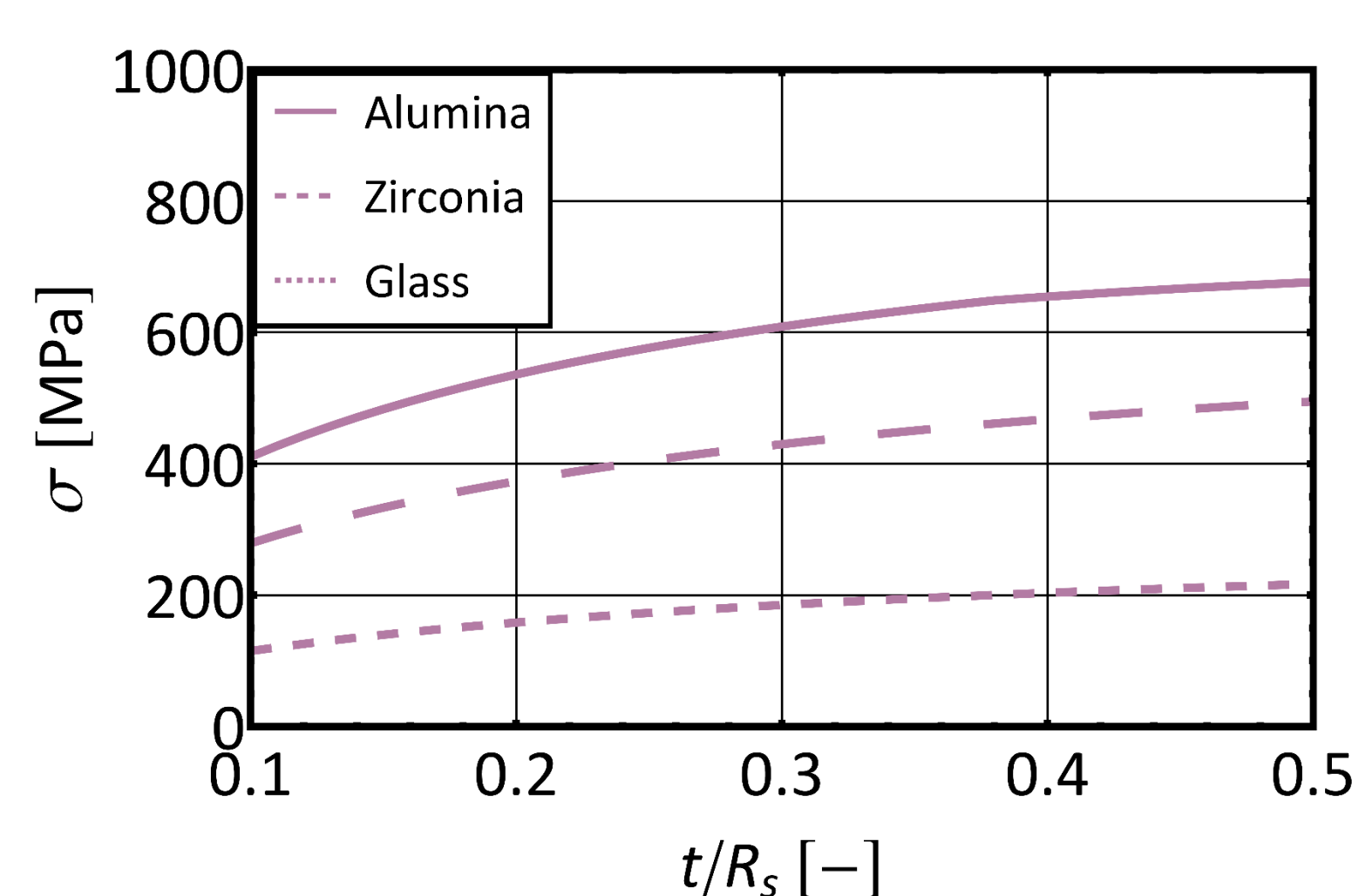
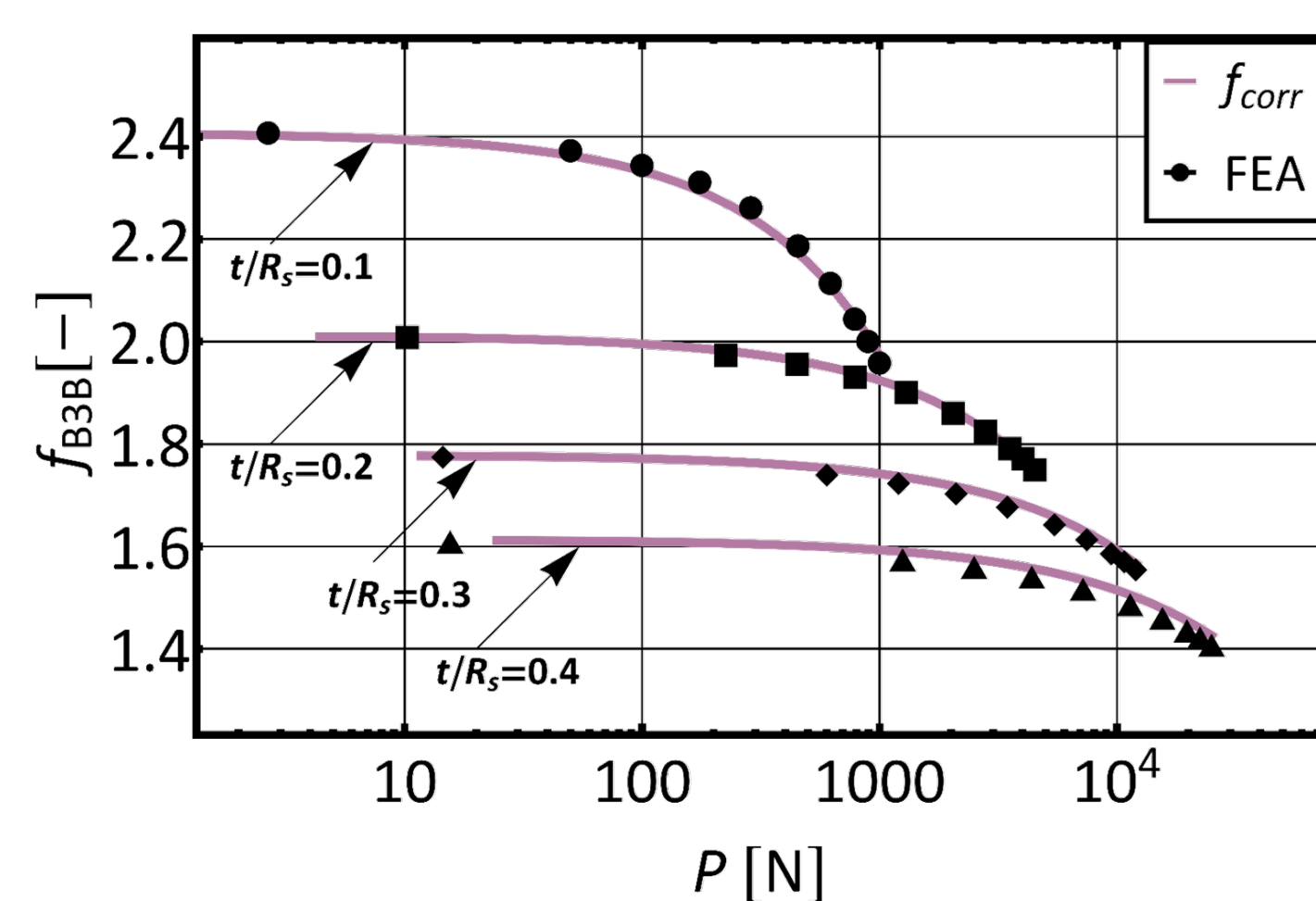
The effect of increasing contact area on f_{B3B} .

RESULTS

A comparison between f_{B3B} determined through contact-based FEA (below) and $f_{B3B, corr}$.



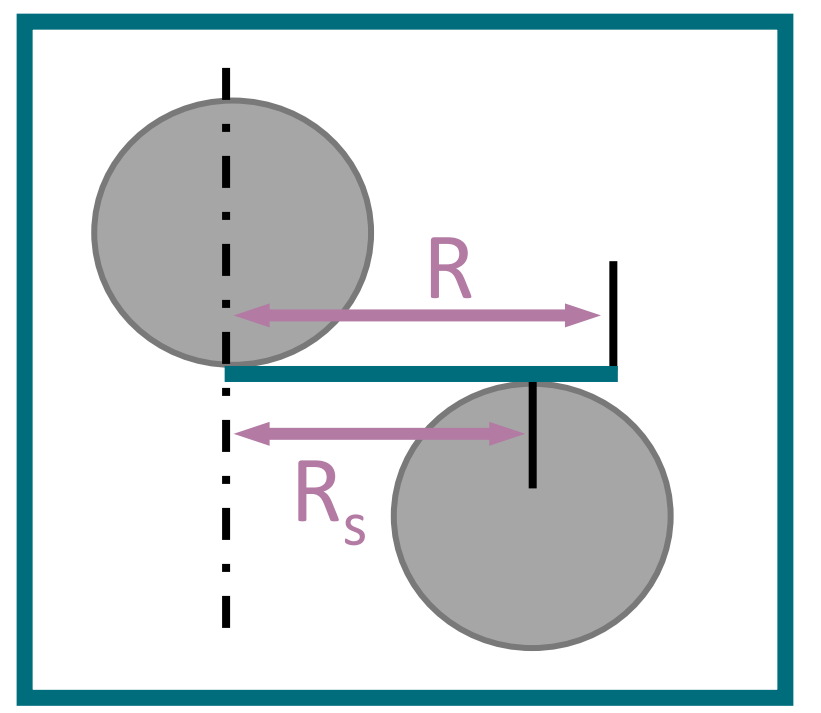
An application range for $f_{B3B, corr}$ was determined, given by the specimen's relative thickness and strength.



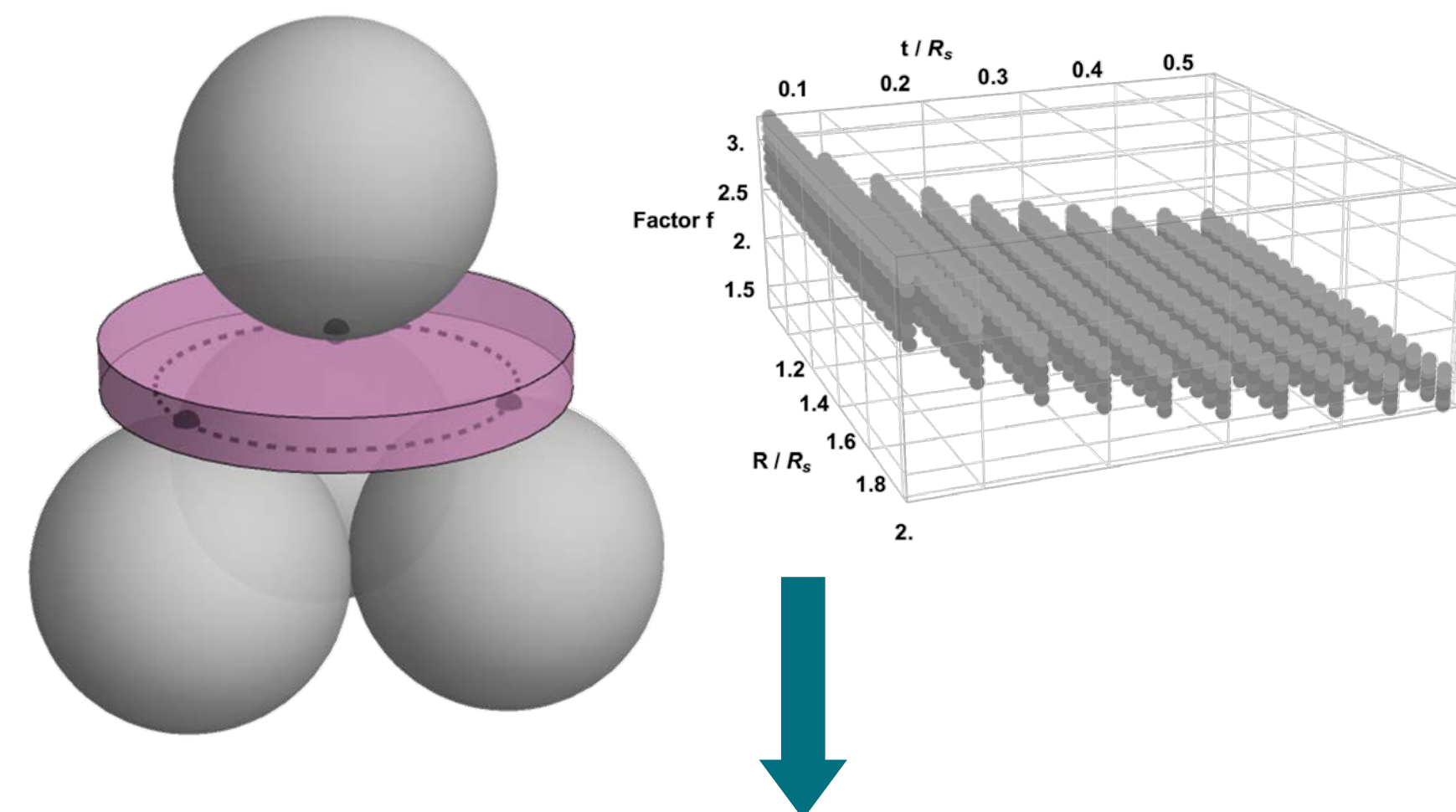
SIMPLIFICATION

$$f\left(\frac{R_s}{R}, \frac{t}{R}, v\right) \rightarrow f\left(\frac{R}{R_s}, \frac{t}{R_s}, v\right)$$

So far, the variables in f_{B3B} were related to R . Relating them to R_s instead greatly improved the "fitability" of FEA data since R_s governs the applied bending moment.



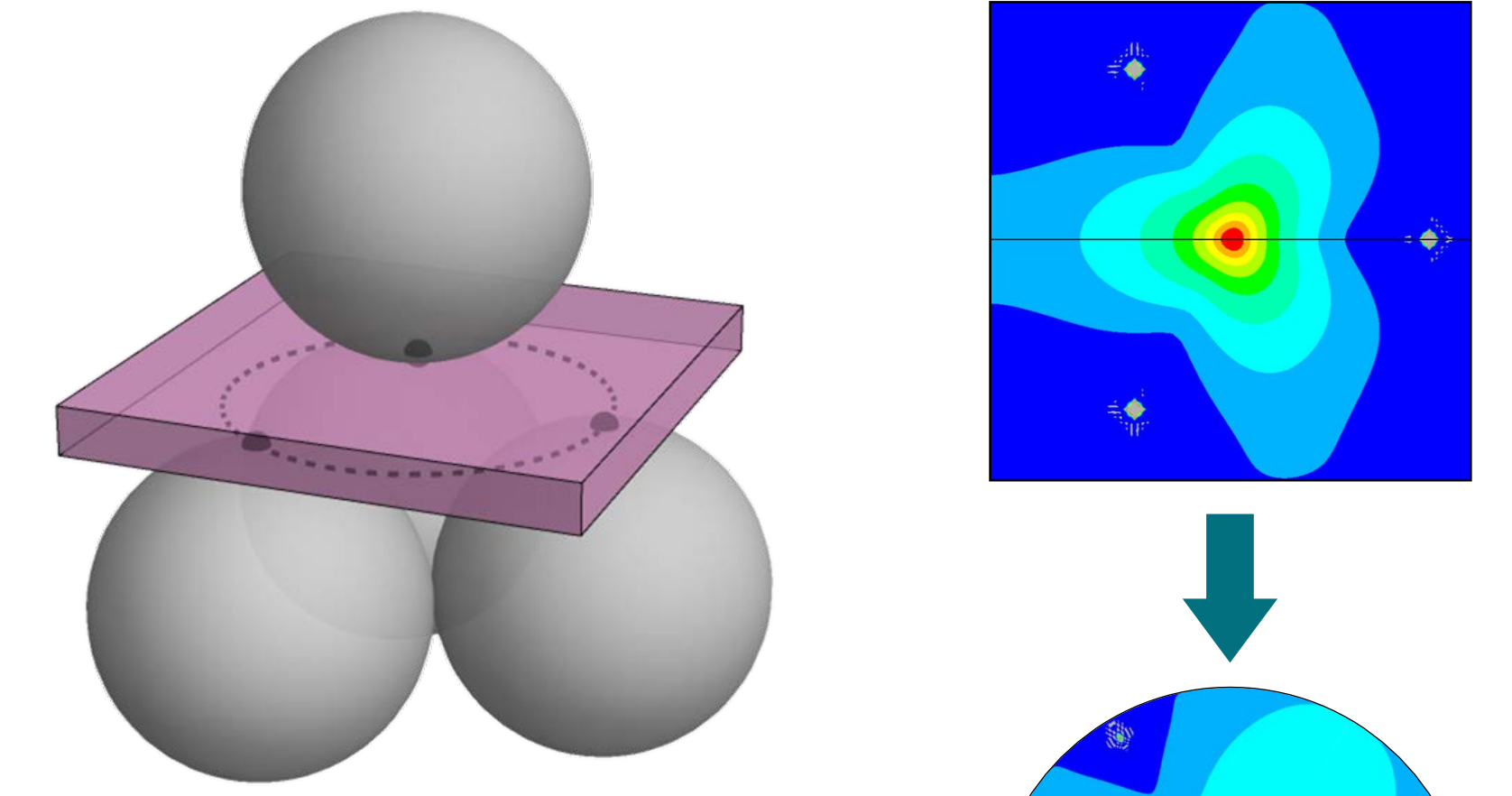
Disc specimen



$$f_{B3B} = \text{Exp} \left[c_1 (1 + v) + c_2 \ln \frac{t}{R_s} + c_3 \sqrt[4]{\frac{R t^2}{R_s^3}} \right]$$
 [3]

A new data-field was generated. The new fit for f_{B3B} of these results is notably shorter whilst retaining the same accuracy.

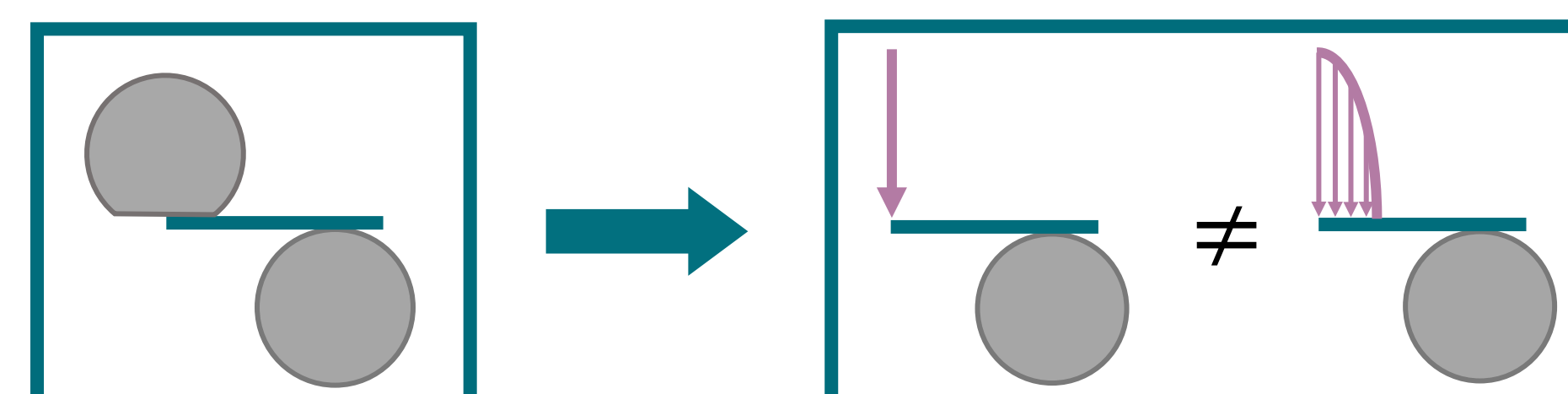
Square specimen



$$D_{eff} = L \left(c_1 + c_2 \frac{L t}{R_s^2} \right)$$

The edge length L is converted to a diameter D_{eff} of an "effective disc" to allow stress evaluation with the new fit for f_{B3B} .

Loading Ball deformation



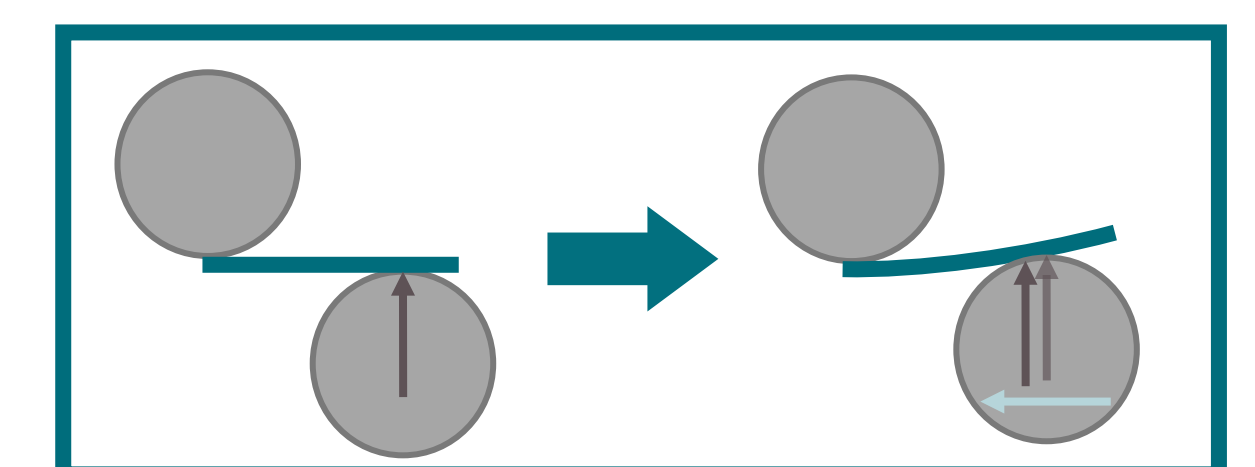
Increasing contact area reduces bending moment

Investigation through a modified FEA model and condensed to a functional expression k_1 .

k_1

$$f_{B3B, corr} = f_{B3B} k_1 k_2$$

Specimen deflection

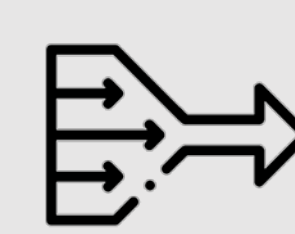


Deflection reduces bending moment

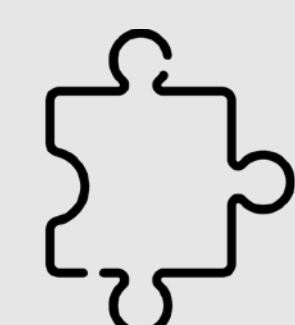
[4] gives an analytical expression for the specimen's deformation to predict the change in bending moment.

k_2

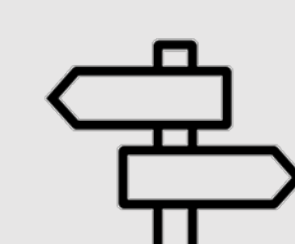
CONCLUSIONS & SUMMARY



The functional expression for f_{B3B} is significantly reduced in length and complexity. The same accuracy as in [2] is achieved.



This simplified expression is extended through a combined analytical and numerical approach by considering ball deformation & specimen deflection.



The application range of the extension k_1 & k_2 is determined and given by the specimen's strength and thickness.

References & Acknowledgments

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- [1] Danzer R. et al., Technische keramische Werkstoffe, (2009)
- [2] Börger A. et al., J. Eur. Ceram. Soc. 22, (2002) 1425–1436
- [3] Staudacher M. et al., J. Eur. Ceram. Soc. 43 (2023) 648–660
- [4] Kirstein A. F. et al., J. Res. Natl. Inst. 70 (1966) 227–244



TO:

$$f_{B3B}(a, b, v) = e^{c_1 (1+v) + c_2 \ln b + c_3 \sqrt[4]{ab^2}}$$

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