

High Speed Casting versus Shell Strength

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The present work discusses the limitation of high speed casting by shell strength. Mould friction data from plant experiments are analysed and compared with measured shell strength from laboratory experiments. The results show, that under regular conditions, mould friction cannot be considered a significant limitation in casting speed. Stability in mould operation should therefore be the key to successful development of continuous casting at highest casting speeds.

Gießgeschwindigkeit und Strangschalenfestigkeit beim Stranggießen von Stahl. Im Rahmen der vorliegenden Arbeit wird die Begrenzung der Gießgeschwindigkeit durch die Festigkeit der Strangschale am Austritt aus der Kokille diskutiert. Die Ergebnisse von Reibungsmessungen an Stranggießanlagen werden analysiert und mit der Strangfestigkeit aus Laborversuchen verglichen. Es zeigt sich, dass unter regulären Verhältnissen und im untersuchten Geschwindigkeitsbereich die Strangfestigkeit keine Limitierung der Gießgeschwindigkeit darstellt. Ziel der Entwicklung des schnellen Gießens sollte somit die Vergleichmäßigung der Bedingungen in der Kokille sein.

1. Introduction

High speed casting (> 4.0 m/min) is a generally pursued target in the development of Continuous Casting (CC) since long time already – for the sake of improved caster productivity and of reduced strand number, realizing a minimum in investment and running costs. As, for instance, documented by the first IISI review, several casters had attained a high speed level in the 1970s, which, however, was difficult to sustain on account of an increased breakout frequency, Fig. 1.

The common reason for high breakout frequency is attributable to *linear* mould tapers generally applied at that time, leading to enhanced gap formation in the corner area followed by corner rotation and off-corner longitudinal cracking in this hot-spot region, but effectively overcome by non-linear (multi- or parabolic) taper^{2,3}. Hence, a renewed attempt of high speed casting is observed since the late 1980s, especially by minimills and regarding both, billet as well as thin slab casting of commercial quality steel products⁴. This has culminated in recent pilot caster trials, attaining 8.0 m/min for slab size

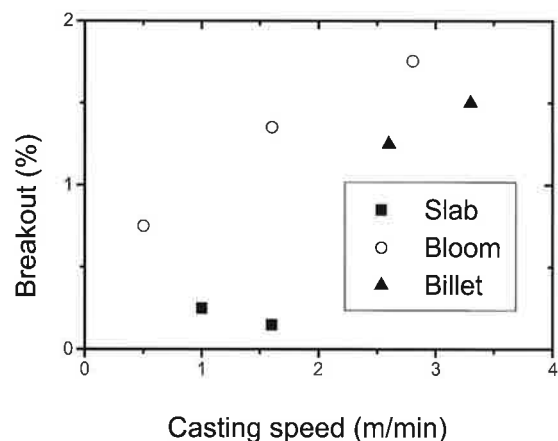
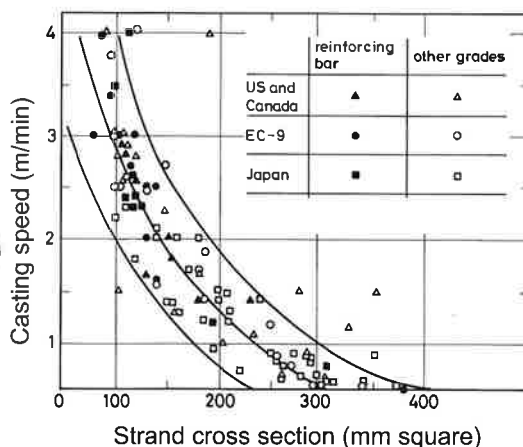


Fig. 1. Casting speed versus cross section (left), and breakout frequency versus casting speed (right) – as reviewed in the 1970s¹

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90 by 1000 mm (followed by liquid core reduction to 50 mm thickness)⁵. Assuming a solidification constant of $K = 16$ mm/min^{0.5} an average shell thickness at mould exit (with an active mould length of 0.8 m in the given case) of 5.1 mm can be derived. Apparently such “thin-wall box” suffices to safely contain the liquid core – provided high uniformity of shell growth in circumferential direction (using for example a parabolic narrow face taper in the given case).

2. Experimental Work

Figure 4 gives a schematic view of the experimental setup. A steel test body, split in two halves, submerges into the liquid steel inside an induction furnace. To form a coherent shell on the (coated) chill body, 2–20 s of holding time are maintained before the lower half is subjected to hydraulic force for about 5 s, which yields strain of 1.6 to 4.0 % and strain rate of $3\text{--}8 \cdot 10^{-3}$ 1/s. Resultant

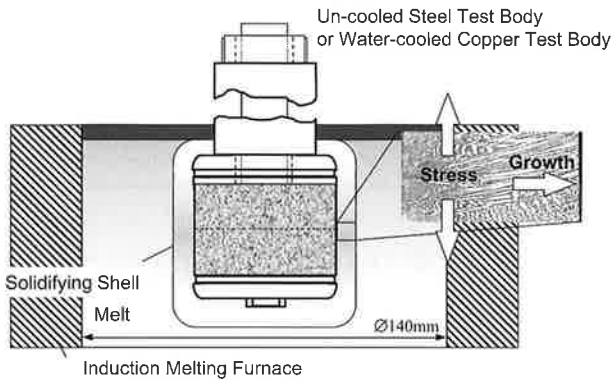


Fig. 4. Schematic presentation of the SSCT test method, geometry of chill body

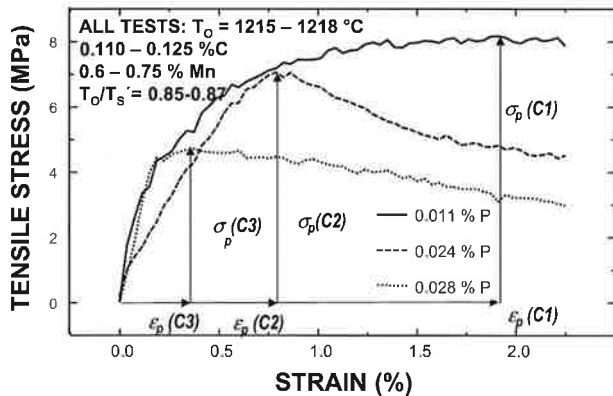


Fig. 5. Example of stress-strain curves in the SSCT test for 0.1 % C – steel and three different P-contents²²

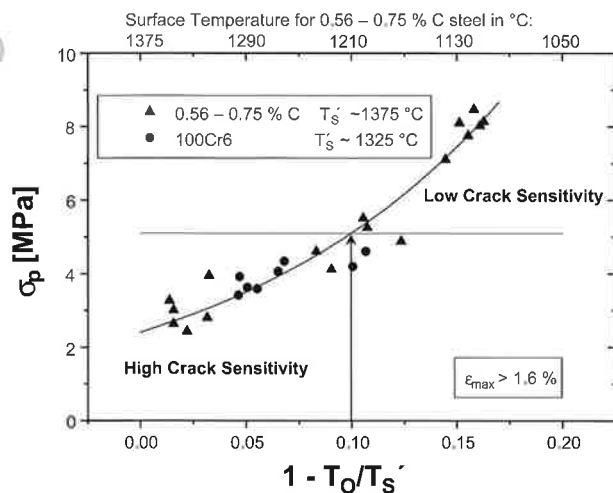


Fig. 6. Maximum shell strength (= peak stress), σ_p of high C-steels in the SSCT test versus homologous temperature (as ratio of T_0 over T_s')

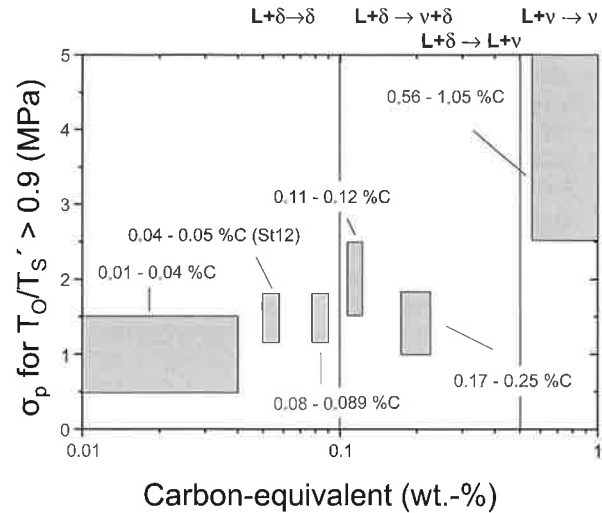


Fig. 7. Meniscus shell strength as a function of steel C-content (log-scale)

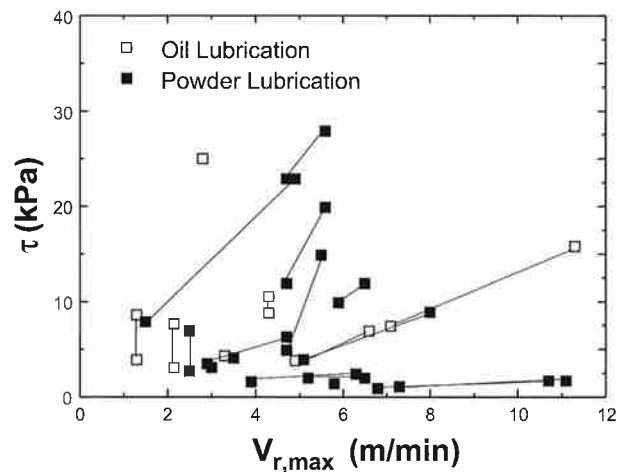


Fig. 8. Measured mould friction data evaluated in ¹² for the relation between maximum relative mould strand/mould velocity and friction shear stress τ

stress-strain curves for the example of 0.1 % C – steel with three different P-contents are shown in Fig. 5.

For high C-steels, shell tearing is observed between the solidus and the homologous temperature $T_0/T_s' > 0.90$, Fig. 6 (with T_0 signifying the shell surface temperature; and T_s' the nonequilibrium solidus temperature including microsegregation), the corresponding range of shell strength (= peak stress), σ_p amounting to 2.5–5.0 MPa. Such tests are performed for a wide range of C-contents with industrial relevance, in order to assess the characteristic meniscus shell strength under CC conditions.

3. Test Results

As a summary of pertinent SSCT-test results, data for the measured peak stress, σ_p near the meniscus i. e. at $T_0/T_s' > 0.90$ are plotted as a function of C-content in Fig. 7, thereby using the “Carbon Equivalent for the Peritectic Reaction” C_p in order to account for the effect of other alloying elements, too.⁹

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